There and Back Again: A heat transfer tale

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Talk Outline

- 0 Setting the scene
- I Status of the code project
- II Thermochemistry development
- III Steady-state accelerator development
- IV Concluding remarks

0. Setting the scene

Update: Simulations of Fire II

Fire II flight test from 1965 is a difficult benchmark problem

- ▶ v= 11km/s, altitude 71 km, capsule size $\approx 1m$
- Lightly radiating ($\approx 10\%$ of the heat load)
- Measurements of total and radiation heat transfer



Where the journey began...



Where it ended



flow solver

Where it ended



The hypersonic blunt body flowfield



Required modelling/technologies

- + shock-fitting
- + high-quality grid generation
- + accelerator for steady-state

+ nonequilibrium (multi-temperature)
thermodynamics

- + nonequilibrium transport properties
- + wall-catalytic boundary conditions
- + finite-rate chemistry (w multi-T

effects)

- + energy exchange mechanisms
- + turbulence modelling
- + surface ablation
- + coupling to radiation field
- + coupling to magnetohydrodynamic effects

Thanks: Daniel Potter

I: Status of the code project -- GDTk

+ core dev team increased from 2 to 4

+ increment in sophistication of

development processes

- + continuous integration testing
- + restructure of repositories (code,

website, docs)

+ moved to github for hosting

Supporting users

- + website
- + documentation:

user guides, reference manuals,

tech notes, catalogue of examples

- + issue tracker
- + Eilmer monthly meet-ups
- + email response to queries
- + face-to-face help
- + version releases





Eilmer Continuous Integration Chronicle

II: Thermochemistry development

$$\begin{split} \frac{\partial}{\partial t} \int_{V} \mathbf{U} \, dV &= -\oint_{S} (\mathbf{F}_{c} - \mathbf{F}_{v}) \cdot \hat{n} \, dA + \int_{V} \mathbf{Q} \, dV \\ \mathbf{U} &= \begin{bmatrix} \vdots \\ \rho e_{v} \end{bmatrix} \\ \mathbf{F}_{i} &= \begin{bmatrix} \vdots \\ \rho e_{v} u \end{bmatrix} \hat{i} + \begin{bmatrix} \vdots \\ \rho e_{v} v \end{bmatrix} \hat{j} + \begin{bmatrix} \vdots \\ \rho e_{v} w \end{bmatrix} \hat{k} \\ \mathbf{V} \text{ibrational excitation} \\ \mathbf{F}_{v} &= \begin{bmatrix} \kappa_{v} \frac{\partial T_{v}}{\partial x} - \sum_{s} \rho h_{vs} D_{s} \frac{\partial Y_{s}}{\partial x} \end{bmatrix} \hat{i} \\ + \begin{bmatrix} \kappa_{v} \frac{\partial T_{v}}{\partial x} - \sum_{s} \rho h_{vs} D_{s} \frac{\partial Y_{s}}{\partial y} \end{bmatrix} \hat{j} \\ + \begin{bmatrix} \kappa_{v} \frac{\partial T_{v}}{\partial x} - \sum_{s} \rho h_{vs} D_{s} \frac{\partial Y_{s}}{\partial y} \end{bmatrix} \hat{k} \\ \mathbf{Q} &= \begin{bmatrix} \vdots \\ \sum_{s} Q^{vib-trans} + \sum_{s} Q^{clec-trans} + \sum_{r} Q^{vib-chem} \end{bmatrix} \\ \end{split}$$

II: Thermochemistry development













```
! Chemkin-style input file
           ! Prepared by: Rowan J. Gollan
           ! Date: 2017-09-23
           1
           ! This is an example to test out the chemkin2eilmer converter.
           ELEMENTS
           Ν
           END
           SPECIES
          N2 N
           END
           REACTIONS
          N2 + N2 <=> N + N + N2
                                        7.00e21 -1.6 224951.04
                                  REV/ 1.09e16 -0.5
                                                       0.0

                                        3.00e22 -1.6
                                                      224951.04
          N2 + N \ll N + N + N
                                  REV/ 2.32e21 -1.5
                                                        0.0
                                                                  /
           END
-- Auto-generated by chemkin2eilmer on: 20-Apr-2022 21:28:28
Config{
   odeStep = {method='alpha-qss'}
Reaction {
        'N2 + N2 <=> N + N + N2',
        fr={'Arrhenius', A=7.000000e+21, n=-1.600000e+00, C=1.132000e+05},
        br={'Arrhenius', A=1.090000e+16, n=-5.000000e-01, C=0.000000e+00},
Reaction{
        'N2 + N <=> N + N + N',
        fr={'Arrhenius', A=3.000000e+22, n=-1.600000e+00, C=1.132000e+05},
        br={'Arrhenius', A=2.320000e+21, n=-1.500000e+00, C=0.000000e+00},
```

}

}

}

top half: transrotational temperature



bottom half: vibroelectronic temperature







2-T dissociating nitrogen model

















2016

[OCT] RJG (7cc267..) : implemented 2D single-block version of Newton-Krylov solver on structured grids, tested on an inviscid Mach 10 flow over a 6 degree wedge.

[NOV] RJG (a27b9e..) : added restarted flexible GMRES and GMRES iterative preconditioner, tested on a Mach 4 laminar flat plate test case [NOV] RJG (0c8bda..) : extended solver to operate on unstructured grids [NOV] RJG (401978..) : shared-memory parallel version

2017

```
[MAR] RJG (b57c0c..) : extended solver to 3D flows
[JUN] RJG (9c28d6..) : extended solver to RANS equations (k-omega
turbulence model)
```

2018

[JUN] KAD (9f1581..) : solver now operates using complex-numbers (complex Frechet derivative variant and complex-step preconditioner) [JUL] KAD (304ef9..) : block-Jacobi preconditioner now operates using complex-step differentiation solver exhibits textbook convergence for the inviscid supersonic ramp test case in the paper by Margues and Pereira [JUL] KAD (7ee999..) : added ILU(0) preconditioner and lagged preconditioner option [SEP] KAD (c58f79..) : re-implemented equation and variable scaling based on Brown and Hindmarsh (1986) paper, improved scaled simulations which were performing poorly [NOV] KAD (f981f8..) : extend precondition matrix construction to 3D ____ 2020 _ _ _ _ [APR] RJG (cfc1bd..) : MPI extension [JUN] KAD (75b697..) : local time-stepping now compatible with Newton-Krylov solver [JUN] KAD (eb6b59..) : user-defined CFL schedule [SEP] KAD (aa1430..) : experimented with matrix-free LU-SGS method as a preconditioner [OCT] KAD (347164..) : extended solver to reacting (finite-rate chemistry) multispecies flows

2021

[APR] KAD (1347d9..) : extended Newton-Krylov solver to operate on solid domains [MAY] KAD (51ed07..) : added multi-temperature capability [JUN] KAD (fcb560..) : spatial order of accuracy of LHS and RHS can be set independently [JUL] KAD (cc0c33..) : added block Symmetric Gauss-Seidel (SGS) preconditioner [AUG] KAD (652e80..) : re-implemented real-valued version using perturbation equation from Knoll's papers [SEP] KAD (082d91..) : added relaxation factor via a physicality check

2022

[FEB] KAD (41140d..) : refactor of Newton-Krylov algorithm to be driven by the physicality check - solver is much more robust now [MAR] KAD (03b9aa..) : finally removed the mass continuity equation for multispecies flows, reacting simulations are much more stable now! [MAR] KAD (cb9ff2..) : added in reverse Cuthill-McKee cell reordering [MAR] KAD (e6514f..) : added in ILU(k) preconditioner



IV: Concluding remarks

Recommended simulation process for estimating heat transfer

- 1. coarse inviscid shock-fitting simulation
- 2. extract grid, tailor and cluster
- 3. coarse viscous simulation
- 4. perform grid refinements



IV: Concluding remarks: does it work?



IV: Concluding remarks

Estimating convective heating for FireII

- + shock-fitting
- + high-quality grid generation
- + accelerator for steady-state
- + nonequilibrium (multi-temperature) thermodynamics
- + nonequilibrium transport properties
- + wall-catalytic boundary conditions
- + finite-rate chemistry (w multi-T effects)
- + energy exchange mechanisms

What's left to do (in the short term) ...

- + generalised 3-T model (Rob Watt)
- + state-specific CO-X model (Nick Gibbons)
- + loosely-coupled CHT simulations (Kyle Damm)
- + coupling to radiation
- +