

Direct Numerical Simulation (DNS) of High-Speed Flows using Graphics Processing Units (GPUs)

CfH Seminar

Christine Mittler

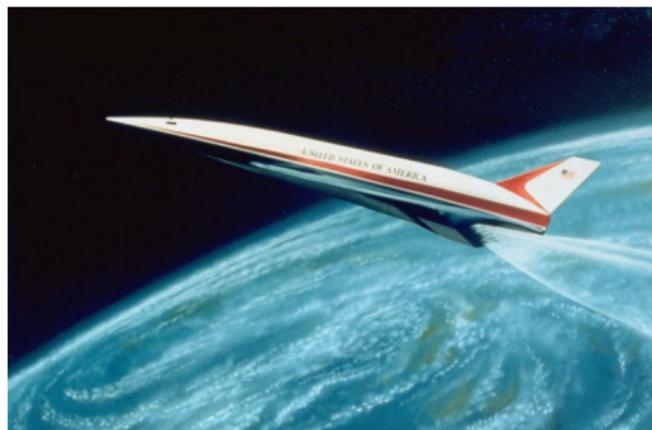
Principal Advisor: Dr Rowan Gollan

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August 1, 2024



- Introduction
 - Motivation
- Flow solver development
 - Proof of concept
 - Objectives
 - Flow solver (Spatz)
 - Verification
 - Performance
- Flat plate investigations

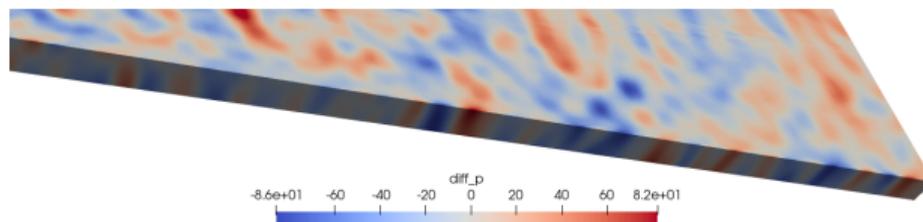
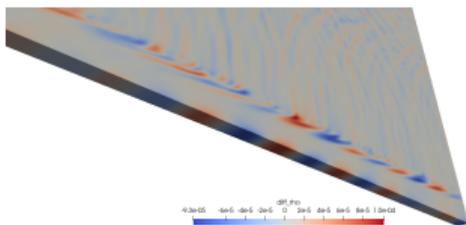
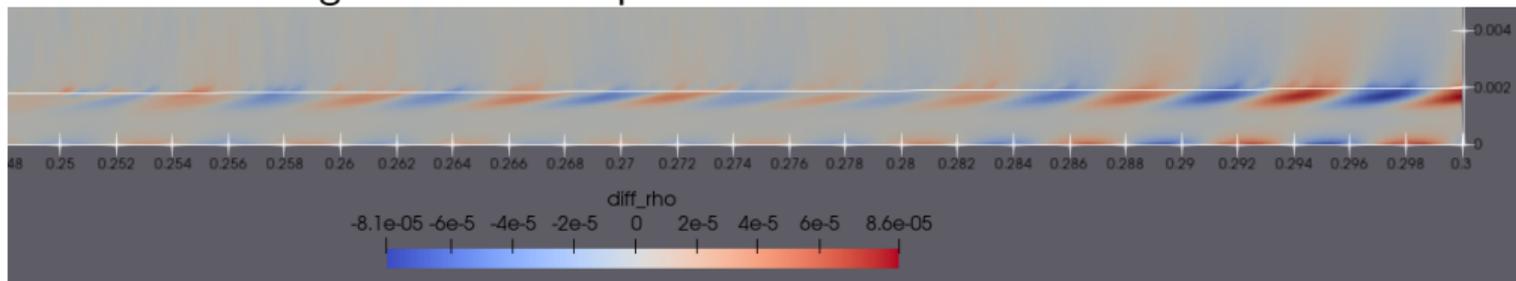


Source:
<https://thehighfrontier.blog/2016/01/02/reagans-impossible-dream-the-x-30-national-aerospace-plane/>

- Predicting transition on hypersonic vehicles one of key challenges in their design
- Transition prediction directly influences estimate of aerodynamic heating and drag
- For National Aerospace Plane (NASP) payload-to-gross-weight ratio nearly doubled depending on how optimistic or conservative predictions of transition were made

- Compared to Reynolds-averaged Navier-Stokes (RANS) and Large Eddy Simulations (LES), direct numerical simulation (DNS) most computationally expensive turbulence simulation technique, but gives highest physical fidelity
- Approach to manage large computational cost of DNS is to improve computational efficiency
 - algorithm enhancement
 - hardware advancement
- Find and develop fluid algorithms best suited to new hardware accelerators
- Graphics Processing Units (GPUs) as hardware accelerators
- Current Literature on DNS on GPUs shows promising speed-ups for certain problem sizes and suitable algorithms
- GPUs dominant choice amongst high performance compute systems across the world

Transition investigation on a flat plate



Flow solver development - Proof-of-concept

Is there a performance benefit for GPUs compared to CPUs for compressible flow simulations?

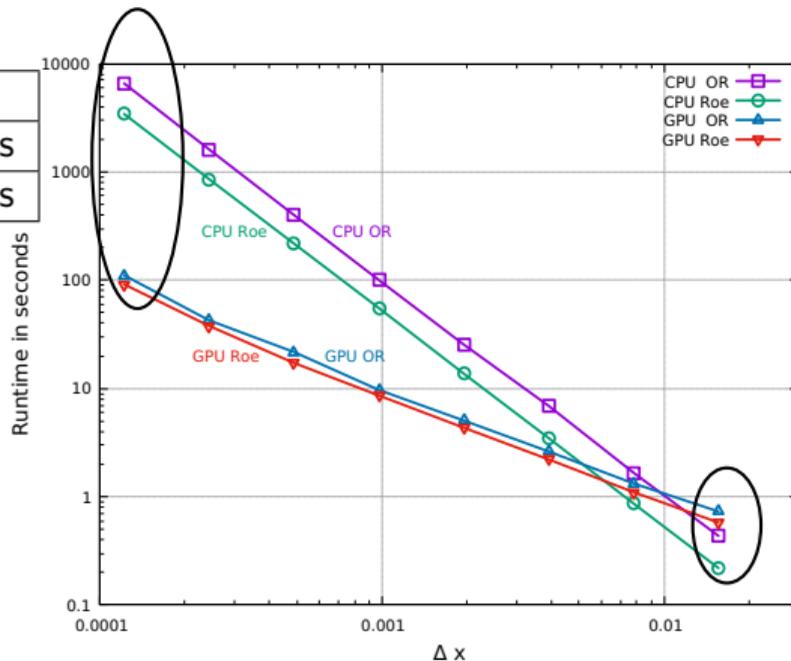
Strategy: Build 1D flow solver and test with two flux calculators on both architectures

8192 cells:

	GPU	CPU
OR	111.01s	6558.33s
Roe	91.33s	3424.68s

Speed-up: 59.1 OR

Speed-up: 37.5 Roe



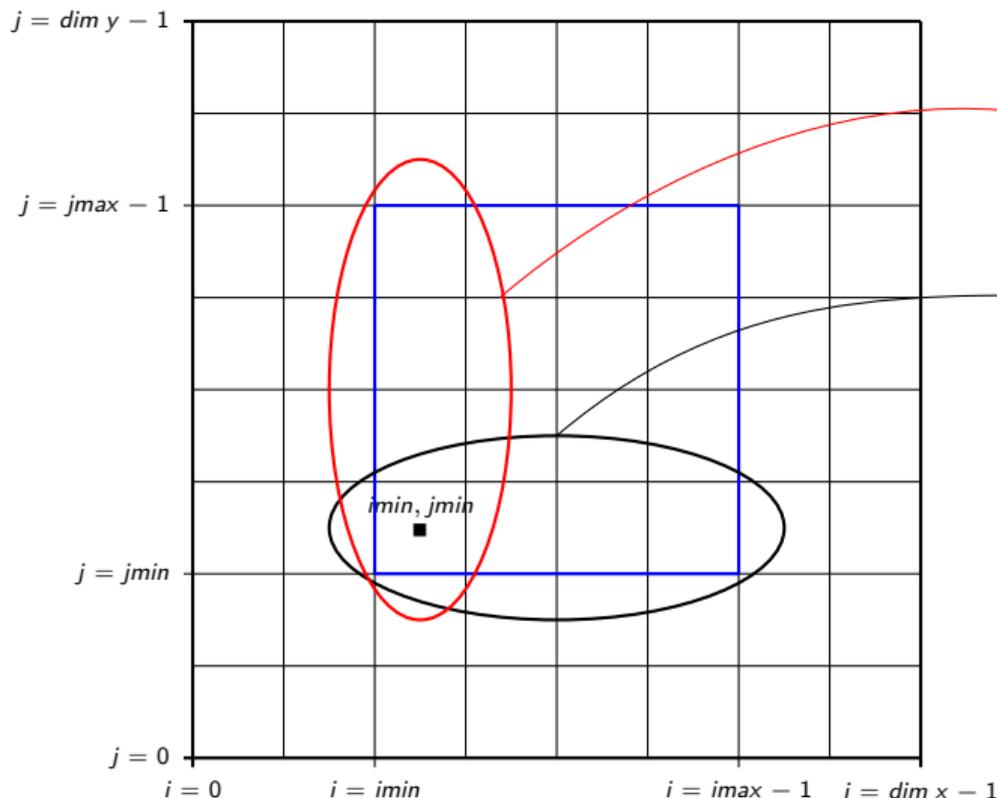
64 cells:

	GPU	CPU
OR	0.73s	0.43s
Roe	0.58s	0.22s

Goals

- Speed-up DNS with GPUs
 - Extend 1D code to 2D/3D on CPU and GPU
 - Test and verify 2D solver
 - Test and verify 3D solver
- Investigate flow physics underlying hypersonic transition
 - Apply GPU solver on heat flux case study

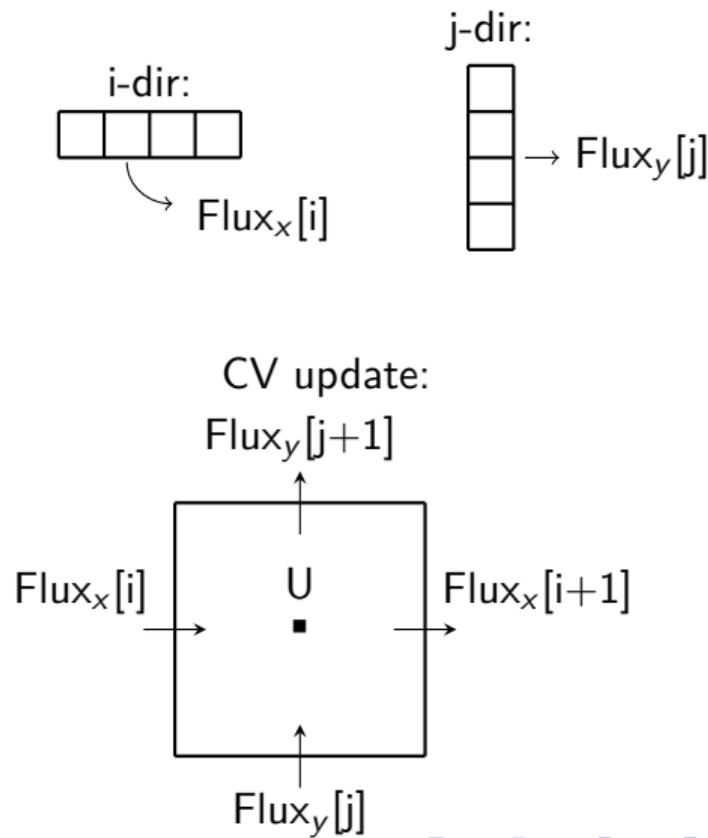
2D / 3D extension from 1D flow solver



- split direction-by-direction and solve like 1D case

CPU Code

- Initialisation (Flow states in cells)
- Start time loop
 - i-dir:
 - Flux calculation
 - j-dir:
 - Transform to local frame
 - Flux calculation
 - Transform to global frame
 - Conserved quantities update
 - Cell average flow properties update
 - Output
- End time loop



Flux calculators in Spatz



Reconstruction - Evolution:

- Approximate Osher-type Riemann (OR) solver
- Roe flux solver

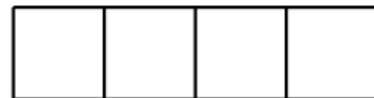


Flux-Solver(L,R) \rightarrow Flux over Face

Flux - Reconstruction:

- Summation-by-parts Alpha-Splitting-Flux (SBP-ASF)

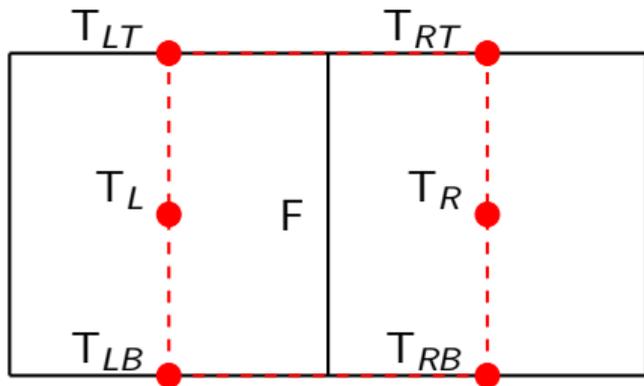
(Direct numerical simulations of instabilities in the entropy layer of a hypersonic blunted slender cone, Whyborn, L., 2023)



Flux-Solver($\square\square\square\square$) \rightarrow Flux over Face

Viscous Flow

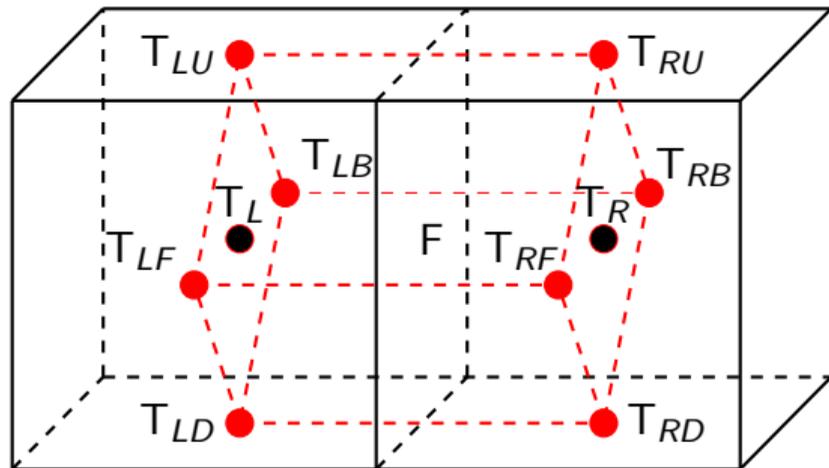
2D viscous flux stencil in x-direction:



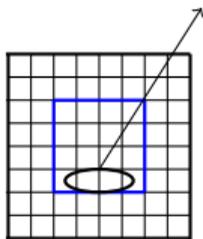
$$\frac{\partial T}{\partial x} = \frac{T_{R-av} - T_{L-av}}{dx}$$

Divergence theorem: $\int_C F \hat{n} dS = \iiint_R \text{div} F dA$

3D viscous flux stencil in x-direction:



$$\frac{\partial T}{\partial x} = \frac{T_{R-av} - T_{L-av}}{dx}$$



Adjustments for GPU implementation

CPU Code (Host)

- Initialisation (Flow states in cells)
- **Memory allocation on GPU**
- **Data transfer to GPU**
- Start time loop
- **Data transfer from GPU**
- Output
- End time loop
- **Free GPU memory**

GPU Code (Device)

- Boundary condition
- Flux calculation
- Conserved quantities update
- Cell average flow properties update

2D

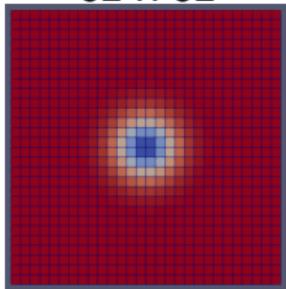
- Isentropic Vortex
- Method of Manufactured solutions (MMS)
 - inviscid
 - viscous
- Self-similar laminar boundary-layer

3D

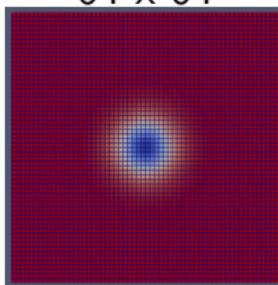
- Method of Manufactured solutions (MMS)
 - inviscid
 - viscous

Simulation of one period

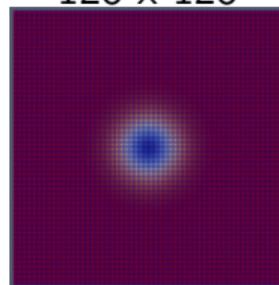
32 x 32



64 x 64

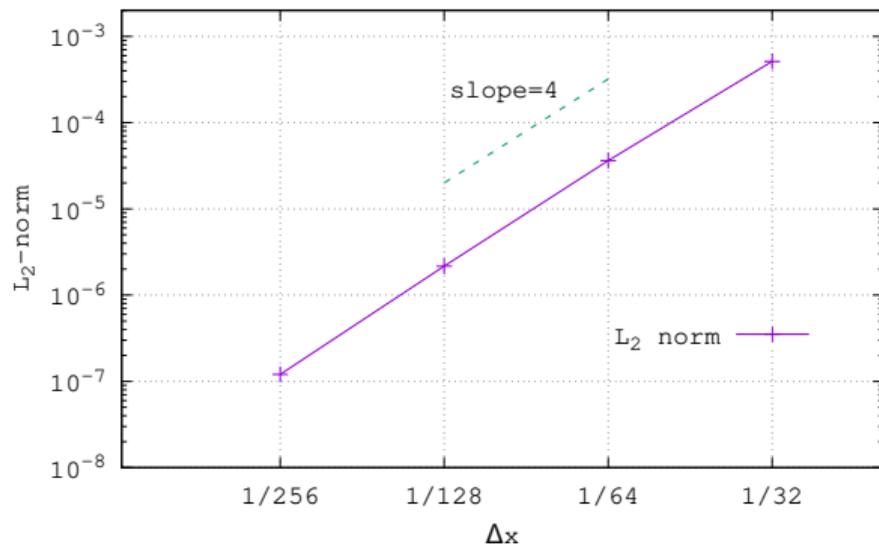


128 x 128



- Simulation of 1 period

Isentropic Vortex - L_2 Norm and Accuracy



$$L_2 = \sqrt{\frac{\sum_{i=0}^N [\text{exact}(i) - \text{solver}(i)]^2}{N}}$$

$$p = \text{LOG}(L_{k+1}/L_k)/\log(r)$$

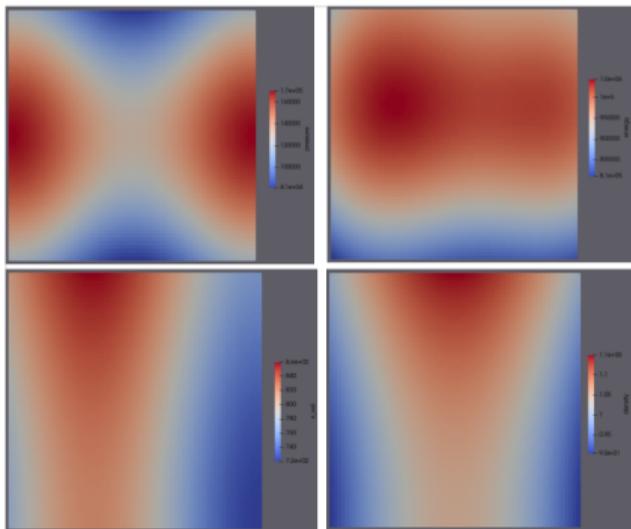
Figure: L_2 -norm density and orders of accuracy p

Process

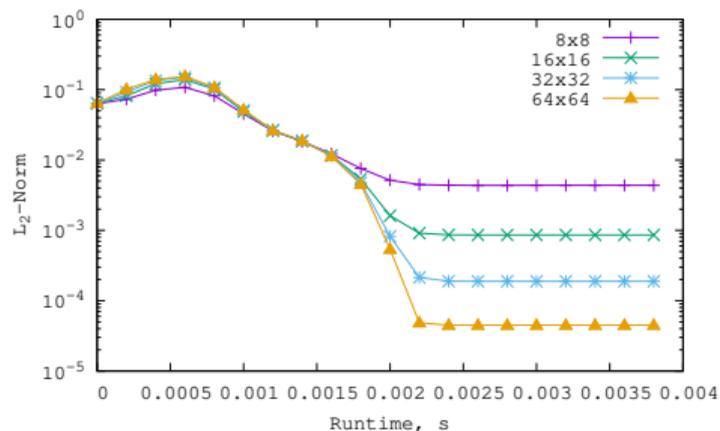
- define analytic solution
- generate source terms using governing equations
- boundary conditions: manufactured solution
- perform simulations with varying grid sizes and compare to exact solution

2D Method of Manufactured solutions (MMS) - inviscid

Simulation results

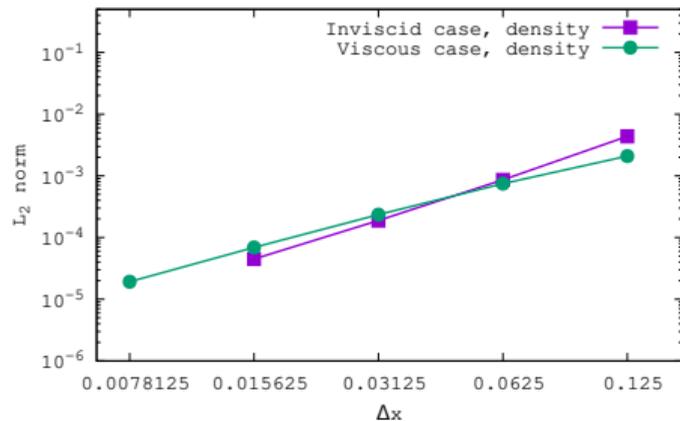


Convergence history - density

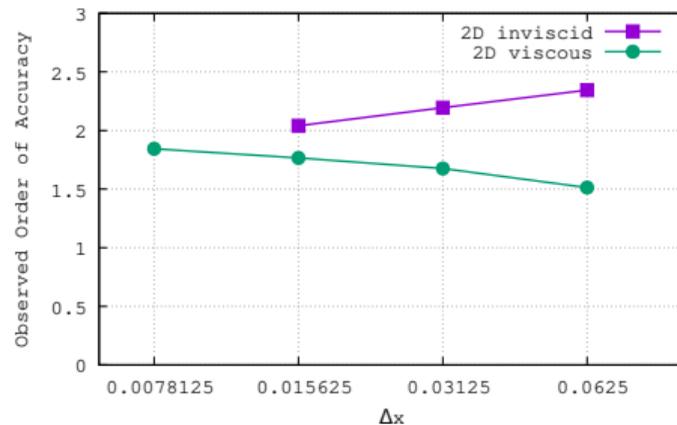


2D Method of Manufactured solutions (MMS) - results

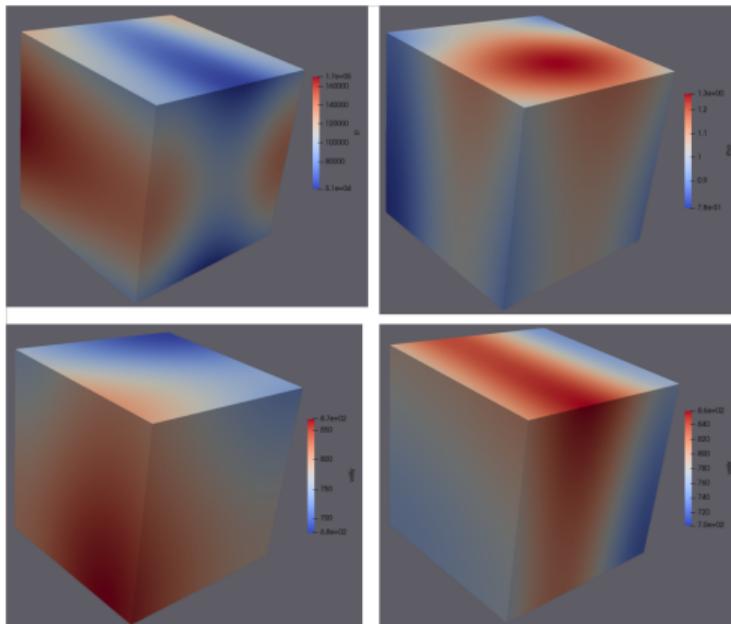
L₂-norm density



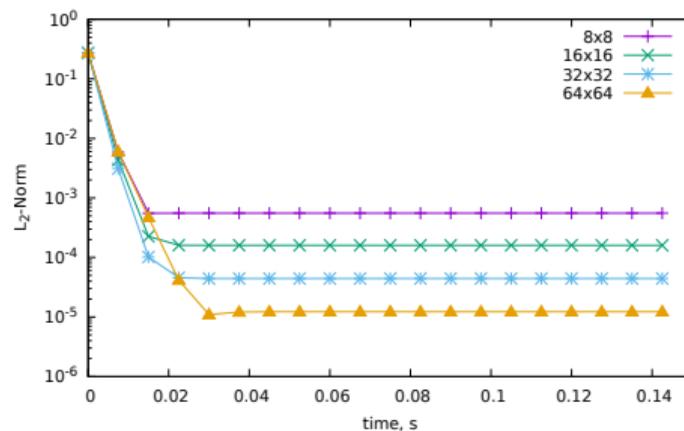
Observed Order of Accuracy



Simulation results (viscous)

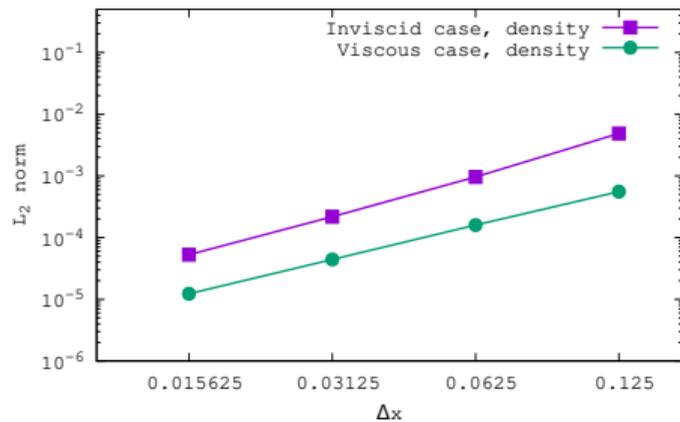


Convergence history - density

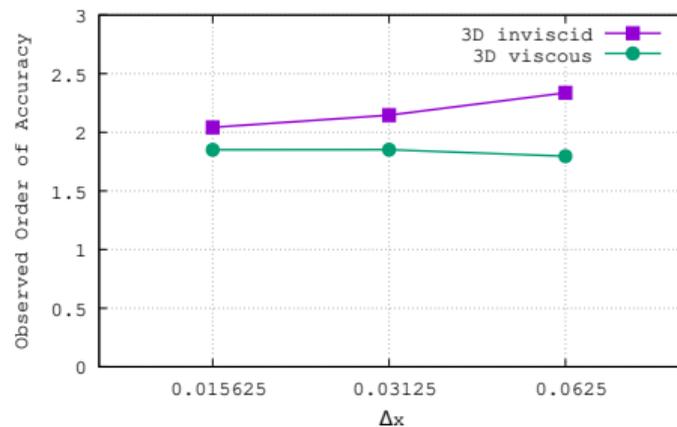


3D Method of Manufactured solutions (MMS) - results

L_2 -norm density

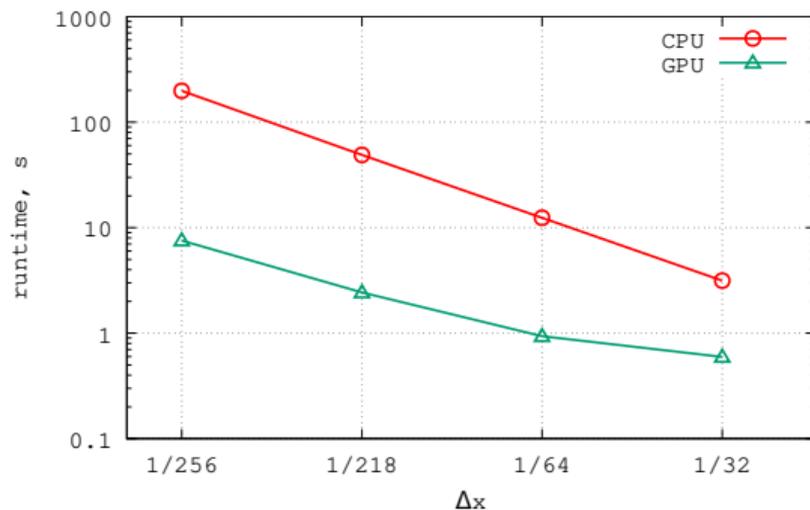
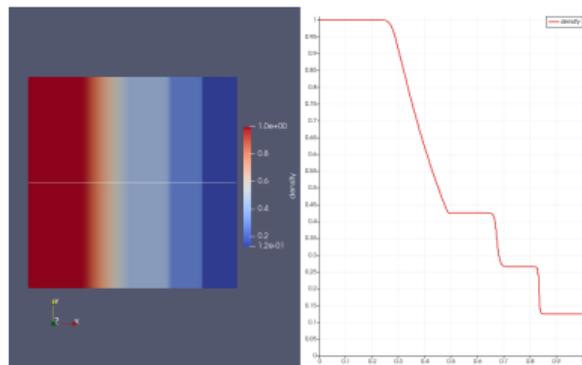


Observed Order of Accuracy



Performance: 2D run-time comparison inviscid flow

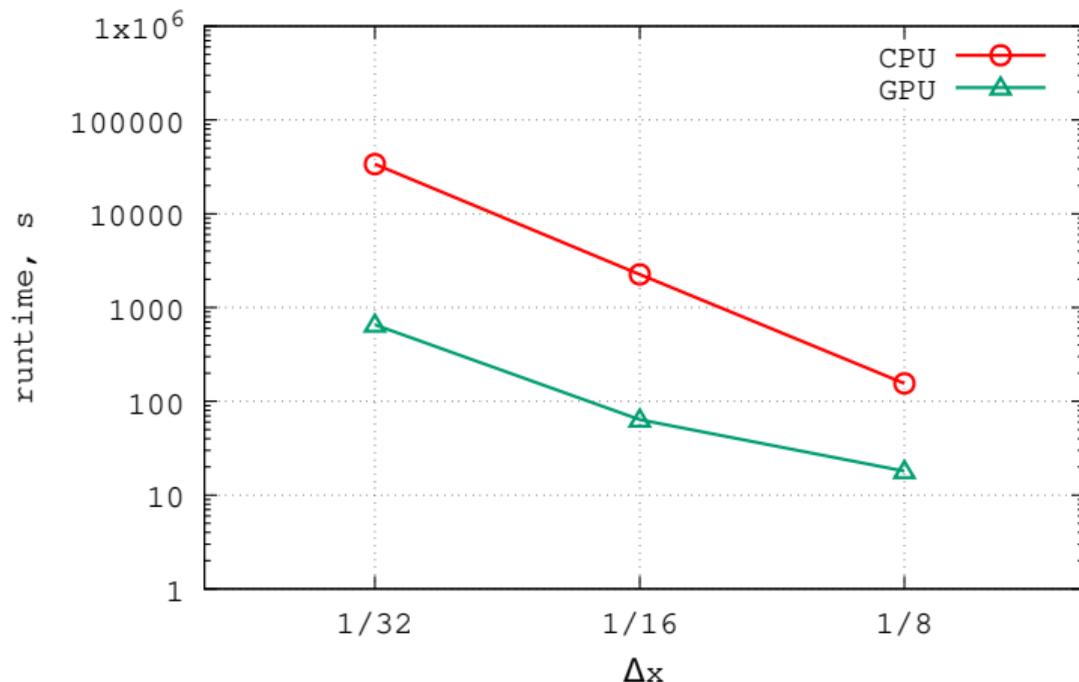
2D Sod's shock tube on CPU (Intel Core i7-4790) and GPU (NVIDIA GeForce GTX 1070)



GPU speed up: 26.3

Performance: 3D run-time comparison viscous flow

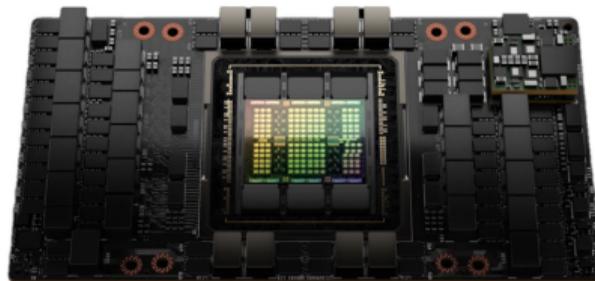
3D viscous MMS on CPU (Intel Core i7-4790) and GPU (NVIDIA GeForce GTX 1070)



GPU speed up: 51.7

Bunya - HPC at UQ

- NVIDIA H100 GPU
- 7 H100 nodes with 3 H100 cards each
- each H100 has 80GB of GPU RAM
- nodes have 2TB of CPU RAM



NVIDIA H100 GPU

Source: <https://resources.nvidia.com/en-us-tensor-core/gtc22-whitepaper-hopper?ncid=no-ncid>

Case study - Flat plate hypersonic transition

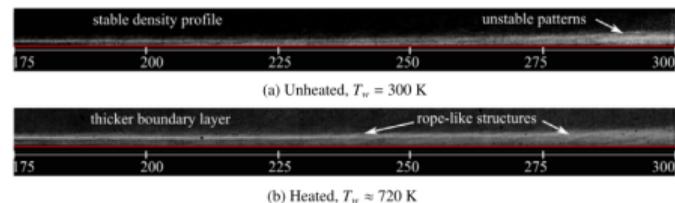
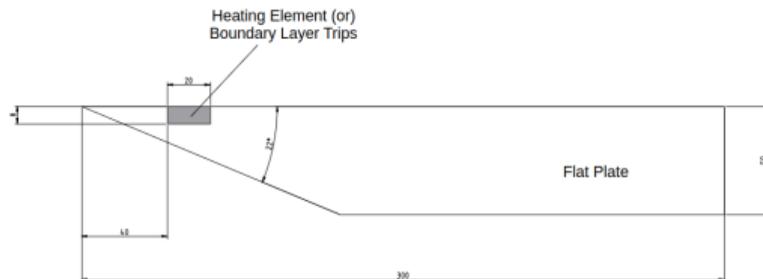


Fig. 18. Flat plate schlieren - Mach 7 enthalpy, $Re_\delta = 5.06 \times 10^6$ 1/m.

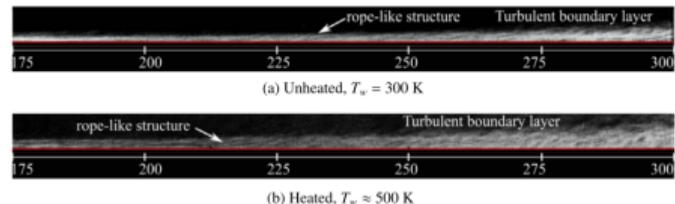


Fig. 19. Flat plate schlieren - Mach 5.5 enthalpy, $Re_\delta = 9.58 \times 10^6$ 1/m.

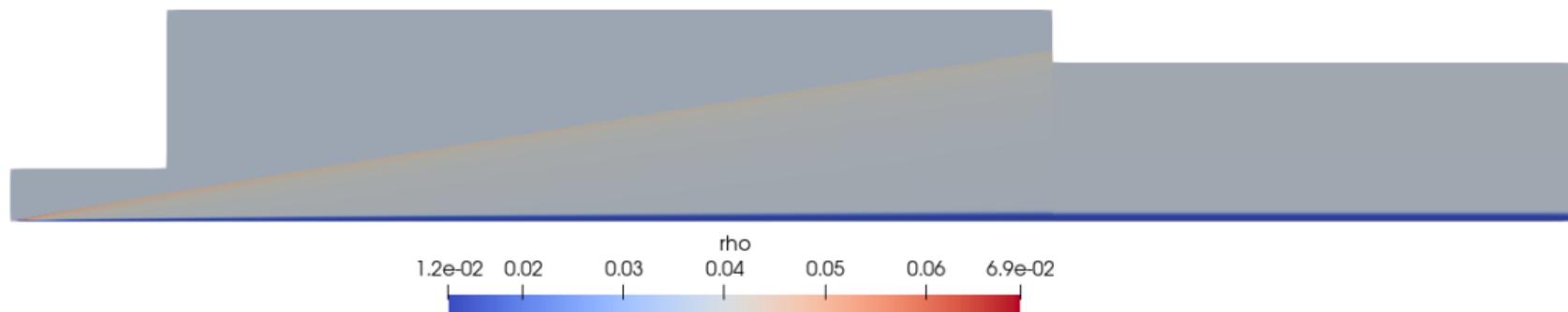
Source: *Electrically-heated flat plate testing in a free-piston driven shock tunnel* Chang, E.W.K., Chan, W.Y.K., Hopkins, K.J., McIntyre, T.J. and Veeraragavan, A. (2020)

Flow properties according to T4 experiments by Eric Chang

Flow parameter	M 7 enthalpy	M 5.5 enthalpy
Pressure	2624	2649
Velocity	2221	1857
Temperature	250	162
Mach	7	7.3
$Re_{unit}(/m)$	$5.06e+06$	$9.58e+06$

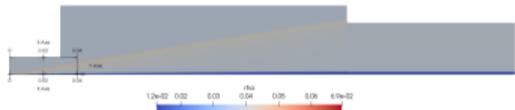
Source: *Electrically-heated flat plate testing in a free-piston driven shock tunnel* Chang, E.W.K., Chan, W.Y.K., Hopkins, K.J., McIntyre, T.J. and Veeraragavan, A. (2020)

Flat plate simulation - stages



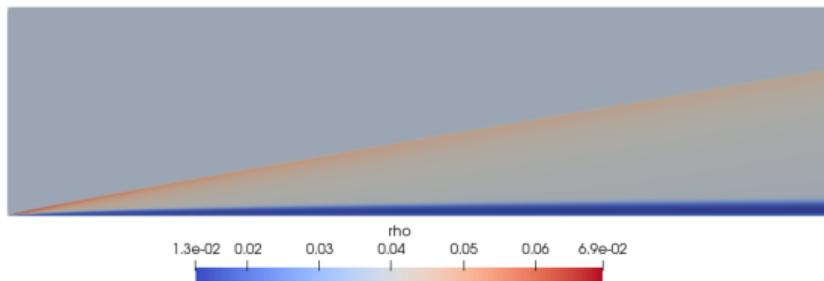
- Stage 0: x: 0-40mm, y: 10mm
- Stage 1: x: 30-200mm, y: 40mm
- Stage 2: x: 175-300mm, y: 30mm

Case study - Stage 0 setup



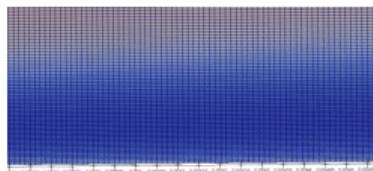
Boundaries

Outflow: linear extrapolation

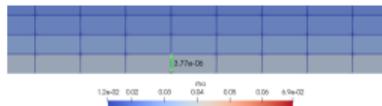


Outflow:
linear
extrapolation

Inflow: Free
stream conditions

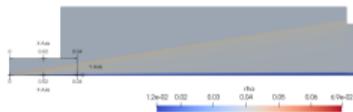


No-slip wall with fixed temperature

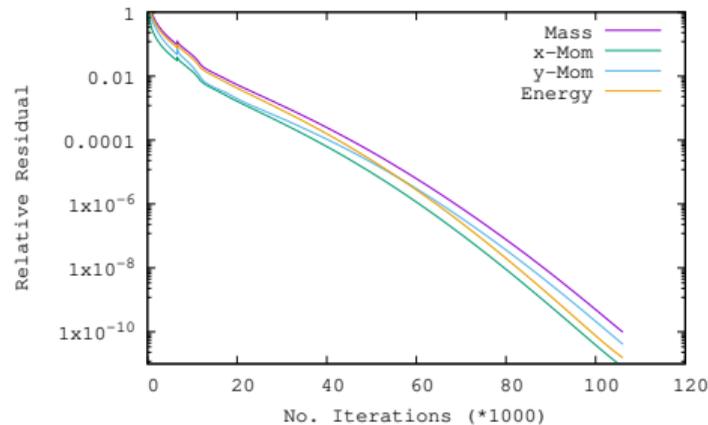


Number of cells in simulation: 2000 x 400

Case study - Stage 0 results

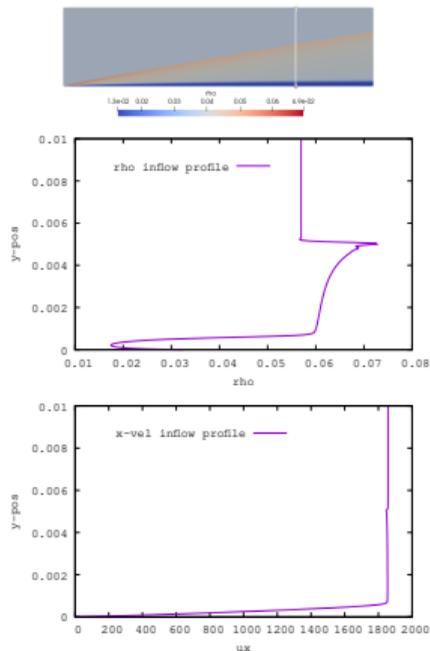


Convergence stage 0

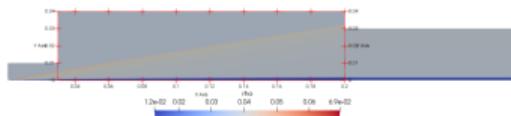


Wall-clock time: 00:47:43

Obtained inflow profile at position $x = 0.03\text{m}$



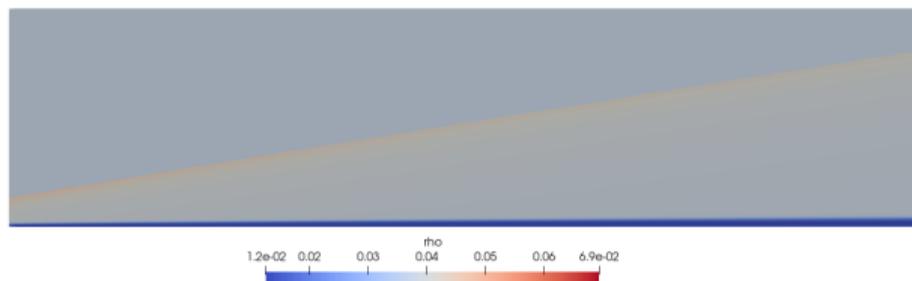
Case study - Stage 1 setup



Boundaries

Outflow: linear extrapolation

Inflow: Profile
from stage 0

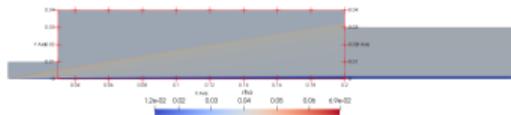


Outflow:
linear
extrapolation

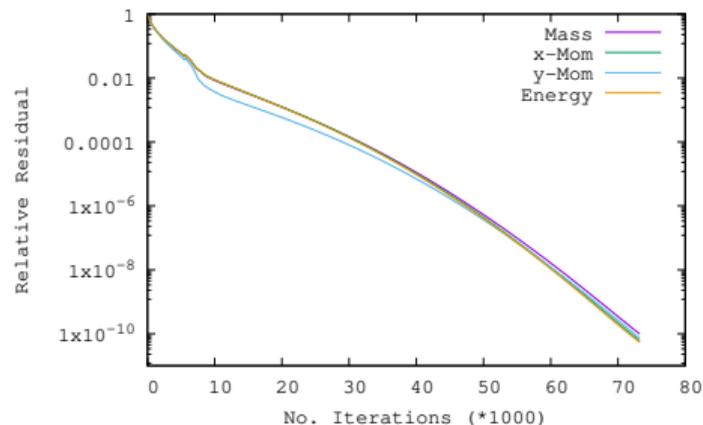
No-slip wall with fixed temperature

Number of cells in simulation: 2800×480

Case study - Stage 1 results

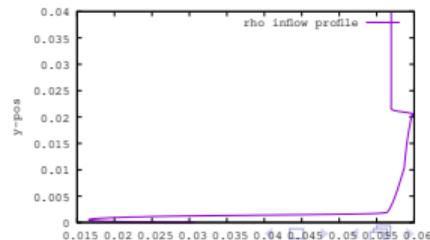
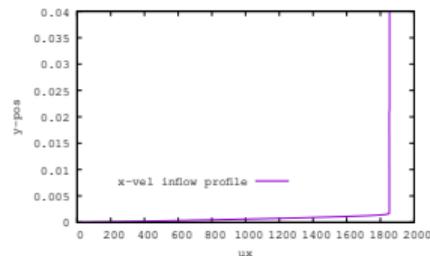
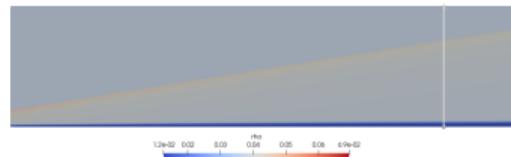


Convergence stage 1

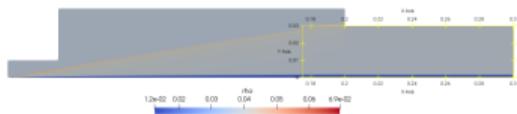


Wall-clock time: 00:17:57

Obtained inflow profile at position $x = 0.175\text{m}$



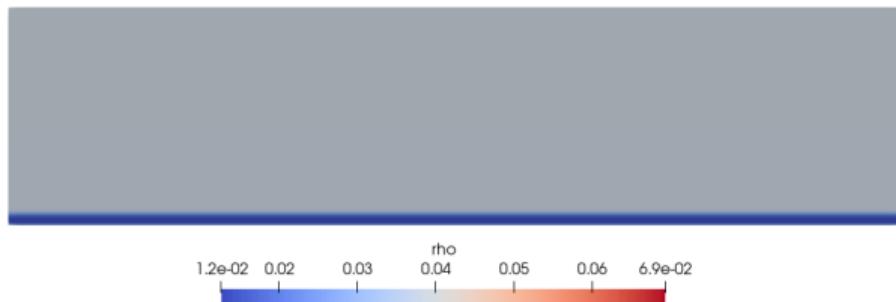
Case study - Stage 2 setup



Boundaries

Outflow: linear extrapolation

Inflow: Profile
from stage 1



Outflow:
linear
extrapolation

No-slip wall with fixed temperature

Number of cells in simulation: 1800×540

Case study - Pressure disturbance

Pressure disturbance according to Johnston and Candler 2022: *Modal analysis of instabilities in the bolt-2 flowfield*:

$$p' = A(2R - 1)$$

$$\rho' = p' \frac{1}{\bar{a}_\infty^2}$$

$$u'_i = p'$$

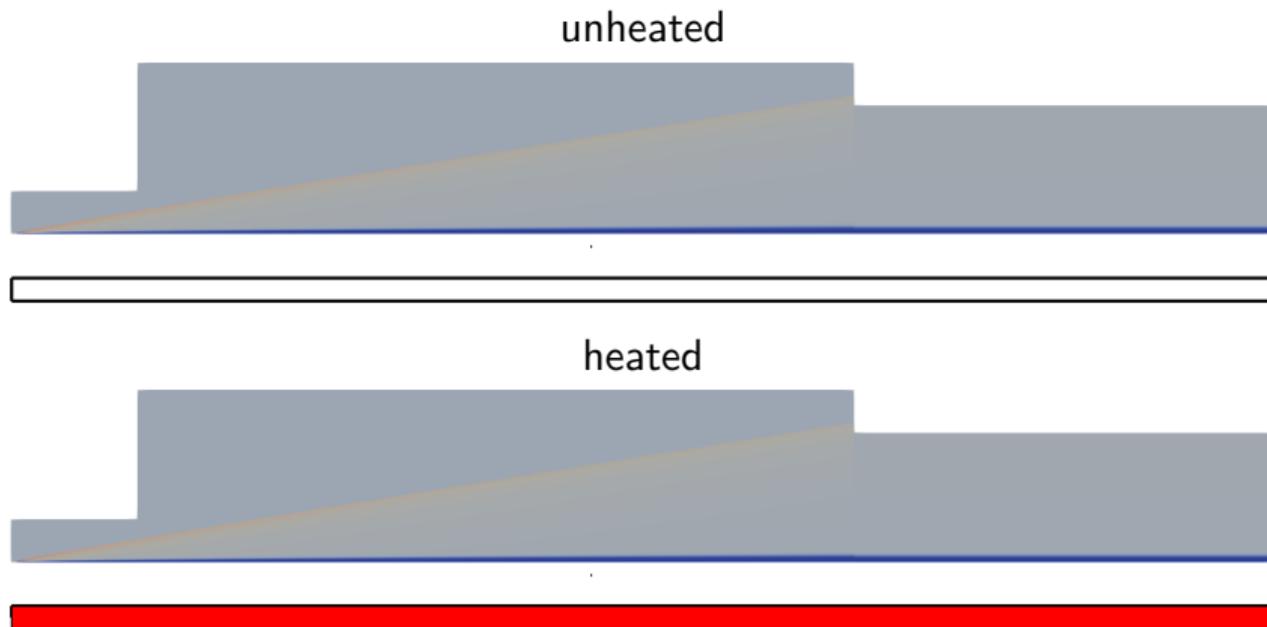
$$T' = p' \frac{(\gamma - 1) \bar{T}}{\bar{\rho} \bar{a}_\infty^2}$$

R: random number between 0 and 1, A: magnitude of white noise disturbance

In this case study (according to T4 white noise measured in experiments):

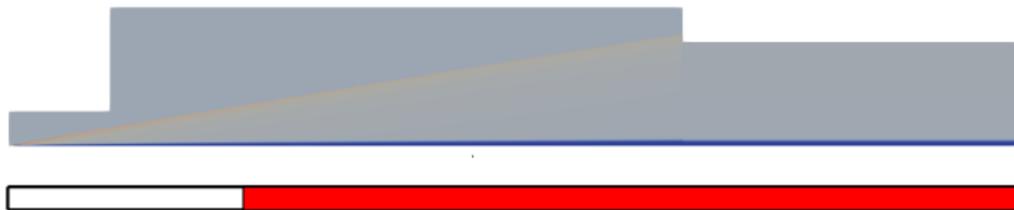
A = 0.7% of free stream pressure

Flat plate heating setups

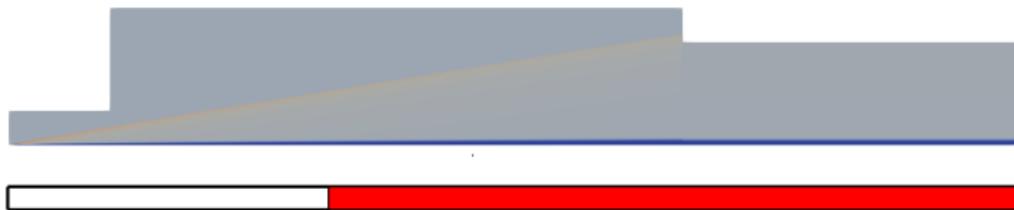


Flat plate heating setups

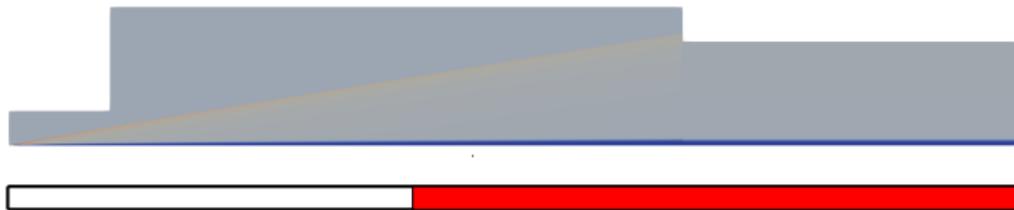
heated at 70mm



heated at 95mm

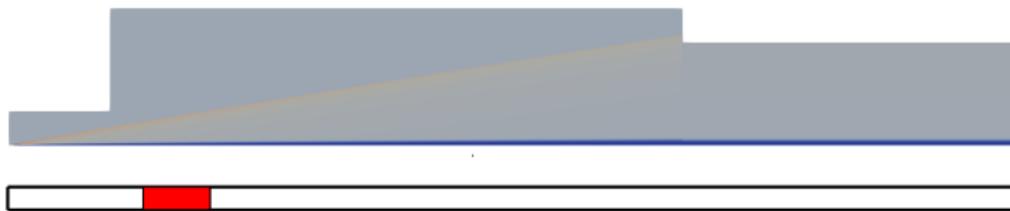


heated at 120mm

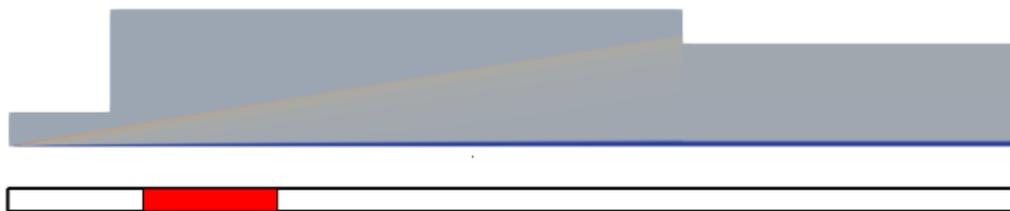


Flat plate heating setups

heated strip - 20mm wide at 40mm



heated strip - 40mm wide at 40mm



Case study - Schlieren results

Schlieren results for Mach 7.3 case

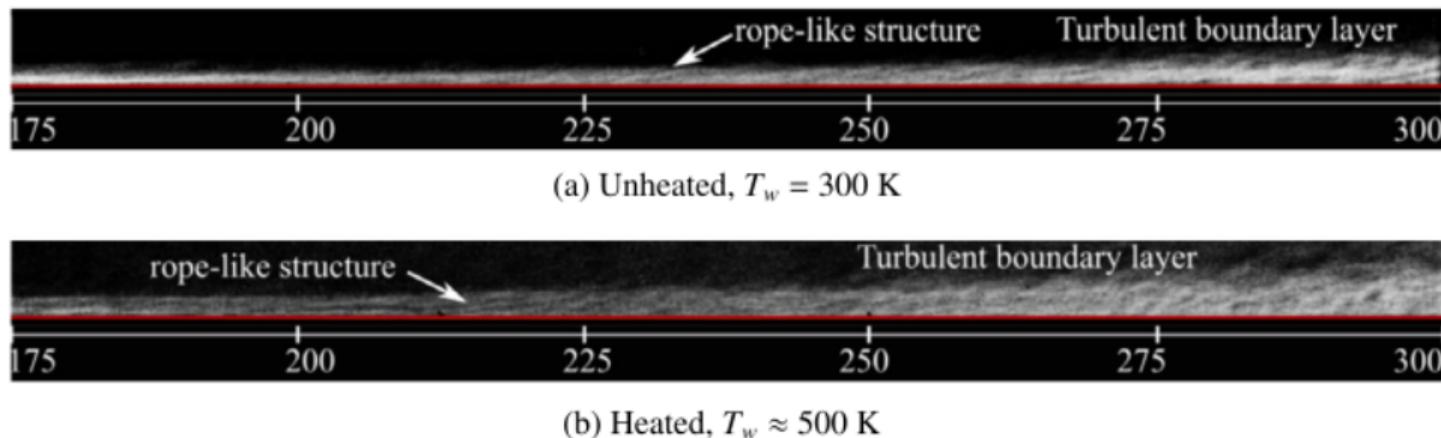
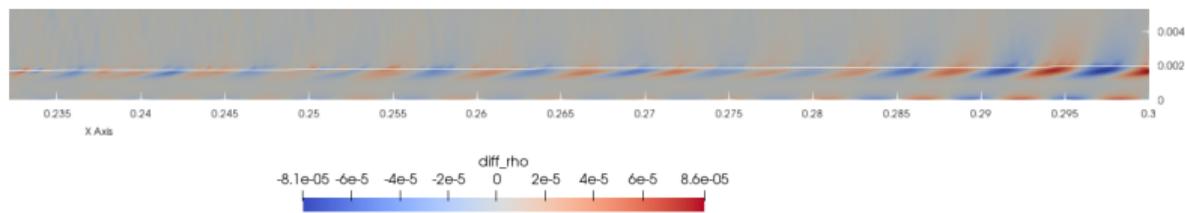


Fig. 19. Flat plate schlieren - Mach 5.5 enthalpy, $Re_u = 9.58 \times 10^6$ 1/m.

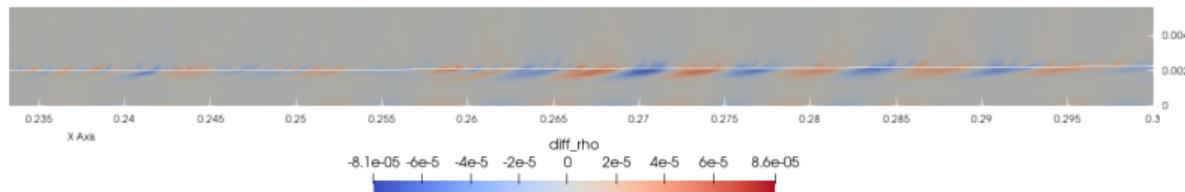
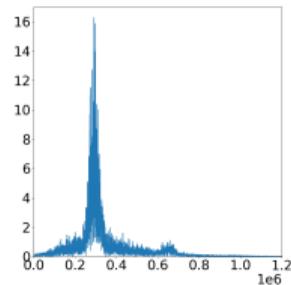
Source: *Electrically-heated flat plate testing in a free-piston driven shock tunnel* Chang, E.W.K., Chan, W.Y.K., Hopkins, K.J., McIntyre, T.J. and Veeraragavan, A. (2020)

DNS results Mach 7.3 - unheated vs fully heated (500K)

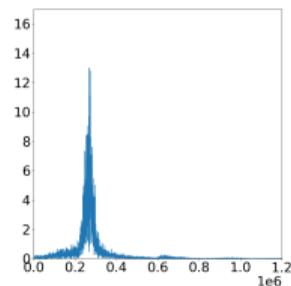
Simulation results for Mach 7.3 case



(a) Unheated flat plate ($T_w = 300\text{K}$)



(b) Heated flat plate ($T_w = 500\text{K}$)



Case study - Schlieren results

Schlieren results for Mach 7 case

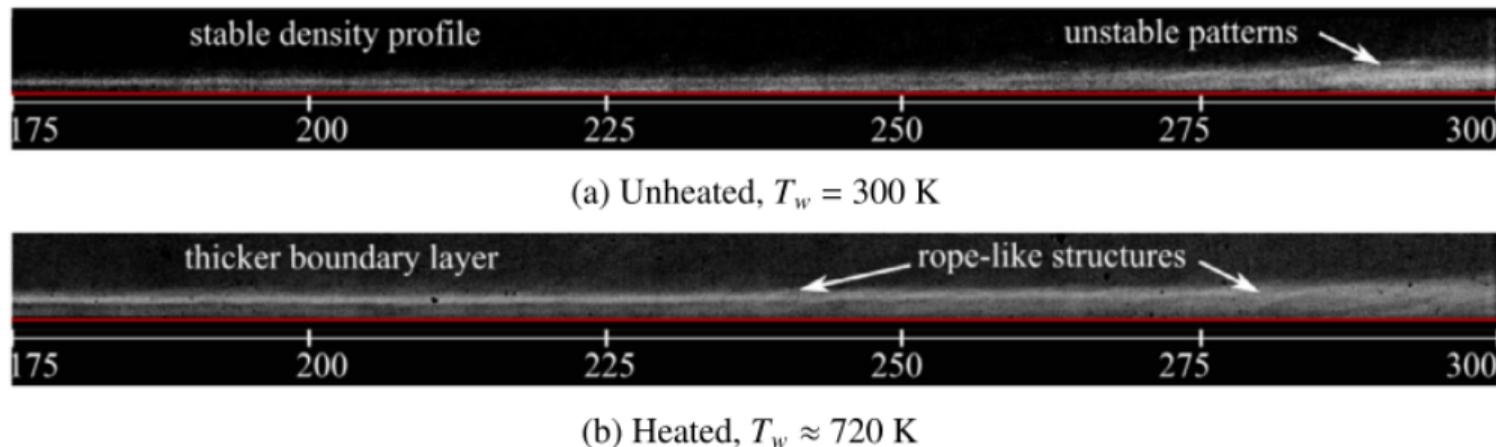
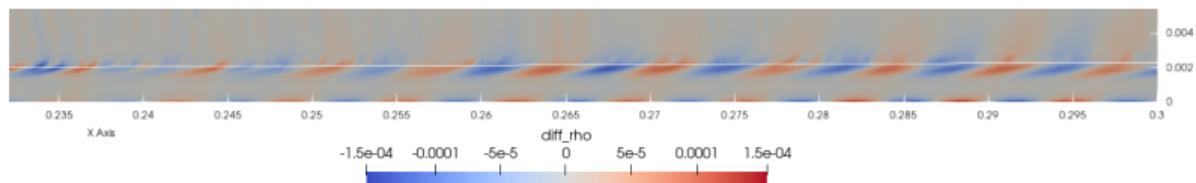


Fig. 18. Flat plate schlieren - Mach 7 enthalpy, $Re_u = 5.06 \times 10^6$ 1/m.

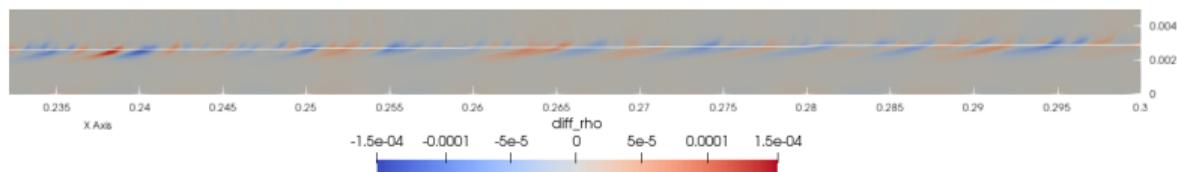
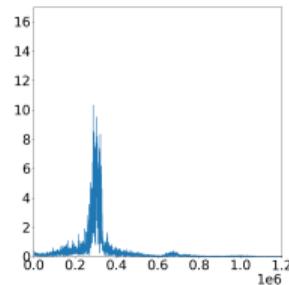
Source: *Electrically-heated flat plate testing in a free-piston driven shock tunnel* Chang, E.W.K., Chan, W.Y.K., Hopkins, K.J., McIntyre, T.J. and Veeraragavan, A. (2020)

DNS results Mach 7 - unheated vs fully heated (825K)

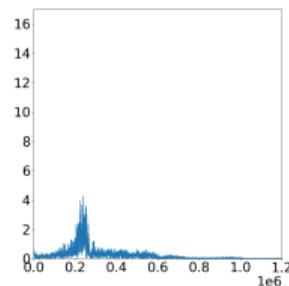
Simulation results for Mach 7 case



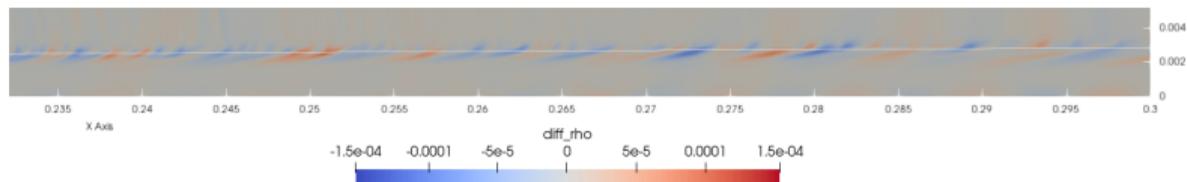
(a) Unheated flat plate ($T_w = 300\text{K}$)



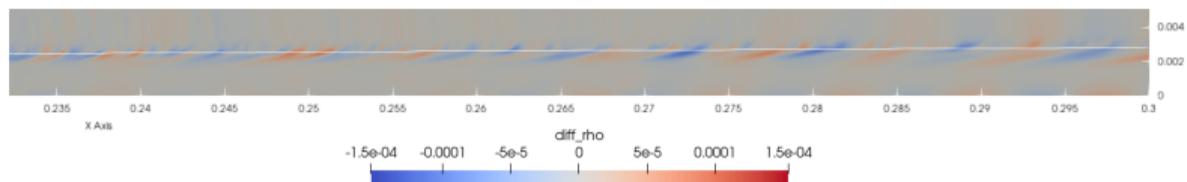
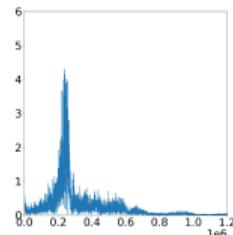
(b) Heated flat plate ($T_w = 825\text{K}$)



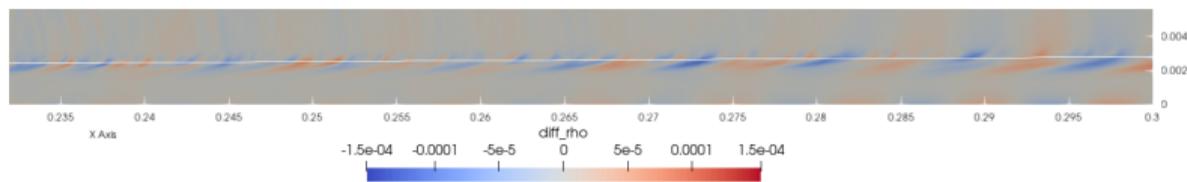
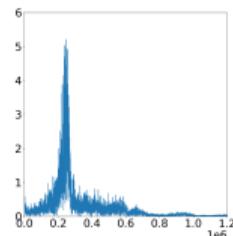
DNS results Mach 7 - partially heated (825K)



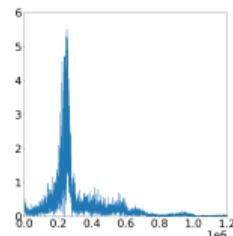
(a) Heated from 70 mm along flat plate



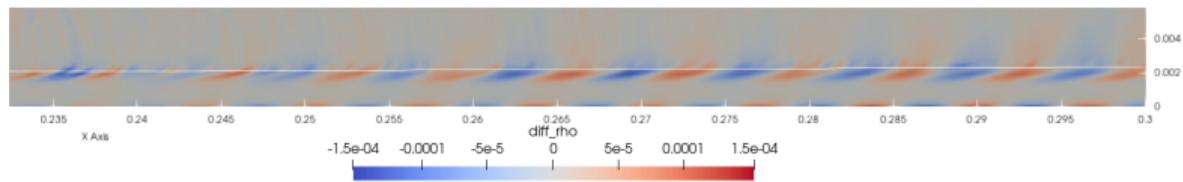
(b) Heated from 95 mm along flat plate



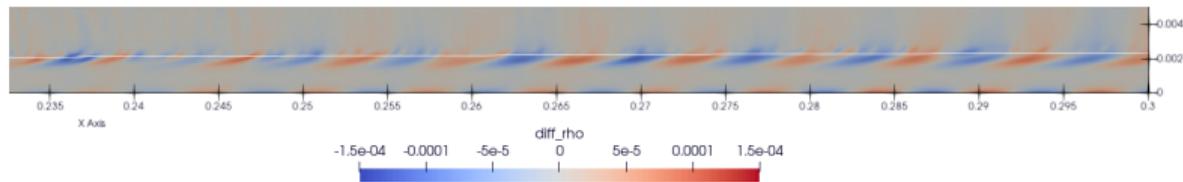
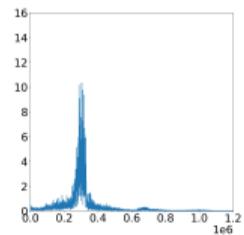
(b) Heated from 120 mm along flat plate



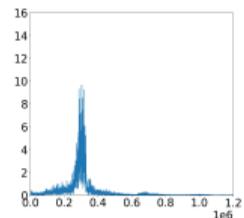
DNS results Mach 7 - heated strips



(a) Heated strip 20mm wide



(b) Heated strip 40mm wide



- GPU code developed
- Verification completed
- Single-GPU enough performance for transition investigation
- Application: unheated and heated flat plate